



SBOS424A-MARCH 2008-REVISED JUNE 2008

Single-Supply, Single-Ended, Precision Programmable Gain Amplifier with MUX

FEATURES

- Rail-to-Rail Input/Output
- Offset: 25μV (typ), 100μV (max)
- Zerø Drift: 0.35μV/°C (typ), 1.2μV/°C (max)
- Low Noise: 12nV/√Hz

(PGA112, PGA116)

- Input Offset Current: ±5nA max (+25°C)
- Gain Error: 0.1% max (G ≤ 32),
 0.3% max (G > 32)
- Binary Gains: 1, 2, 4, 8, 16, 32, 64, 128
- Scope Gains: 1, 2, 5, 10, 20, 50, 100, 200 (PGA113, PGA117)
- Gain Switching Time: 200ns
- Two Channel MUX: PGA112, PGA113 10 Channel MUX: PGA116, PGA117
- Four Internal Calibration Channels
- Amplifier Optimized for Driving CDAC ADCs
- Output Swing: 50mV to Supply Rails
- AV_{DD} and DV_{DD} for Mixed Voltage Systems
- I_Q = 1.1mA (typ)
- Software/Hardware Shutdown: I_Q ≤ 4μA (typ)
- Temperature Range: -40°C to +125°C
- SPI™ Interface (10MHz) with Daisy-Chain Capability

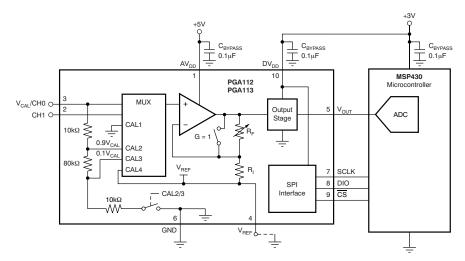
APPLICATIONS

- Remote e-Meter Reading
- Automatic Gain Control
- Portable Data Acquisition
- PC-Based Signal Acquisition Systems
- Test and Measurement
- Programmable Logic Controllers
- Battery-Powered Instruments
- Handheld Test Equipment

DESCRIPTION

The PGA112 and PGA113 (binary/scope gains) offer two analog inputs, a three-pin SPI interface, and software shutdown in an MSOP-10 package. The PGA116 and PGA117 (binary/scope gains) offer 10 analog inputs, a four-pin SPI interface with daisy-chain capability, and hardware and software shutdown in a TSSOP-20 package.

All versions provide internal calibration channels for system-level calibration. The channels are tied to GND, $0.9V_{CAL}$, $0.1V_{CAL}$, and V_{REF} , respectively. V_{CAL} , an external voltage connected to Channel 0, is used as the system calibration reference. Binary gains are: 1, 2, 4, 8, 16, 32, 64, and 128; scope gains are: 1, 2, 5, 10, 20, 50, 100, and 200.



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This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

PACKAGE AND MODEL COMPARISON

	# OF MUX		SPI	SHUT			
DEVICE	INPUTS	GAINS (Eight Each)	DAISY-CHAIN	HARDWARE	SOFTWARE	PACKAGE	
PGA112	Two	Binary	No	No	✓	MSOP-10	
PGA113	Two	Scope	No	No	✓	MSOP-10	
PGA116	10	Binary	✓	✓	✓	TSSOP-20	
PGA117	10	Scope	✓	✓	✓	TSSOP-20	

ORDERING INFORMATION(1)

PRODUCT	DESCRIPTION (Gains/Channels)	PACKAGE-LEAD	PACKAGE DESIGNATOR	PACKAGE MARKING	
PGA112	Binary (2)/2 Channels	MSOP-10	DGS	P112	
PGA113	Scope (3)/2 Channels	MSOP-10	DGS	P113	
PGA116 ⁽⁴⁾	Binary ⁽²⁾ /10 Channels	TSSOP-20	PW	PGA116	
PGA117 ⁽⁴⁾	Scope (3)/10 Channels	TSSOP-20	PW	PGA117	

⁽¹⁾ For the most current package and ordering information see the Package Option Addendum at the end of this document, or see the TI web site at www.ti.com.

ABSOLUTE MAXIMUM RATINGS(1)

Over operating free-air temperature range, unless otherwise noted.

		PGA112, PGA113, PGA116, PGA117	UNIT				
Supply Voltage		+7	V				
Signal Input Terr	minals, Voltage ⁽²⁾	GND – 0.5 to (AV _{DD}) + 0.5 V					
Signal Input Terr	minals, Current ⁽²⁾	±10	· ==:				
Output Short-Cir	cuit	Continuous	Continuous				
Operating Temp	erature	-40 to +125	°C °C				
Storage Temper	ature	-65 to +150	°C				
Junction Temper	rature	+150	°C				
	Human Body Model (HBM)	3000	V				
ESD Ratings:	Charged Device Model (CDM)	1000	V				
	Machine Model (MM)	300	V				

⁽¹⁾ Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those specified is not implied.

⁽²⁾ Binary gains: 1, 2, 4, 8, 16, 32, 64, and 128.

⁽³⁾ Scope gains: 1, 2, 5, 10, 20, 50, 100, and 200.

⁽⁴⁾ Available Q3 2008.

⁽²⁾ Input terminals are diode-clamped to the power-supply rails. Input signals that can swing more than 0.5V beyond the supply rails should be current limited to 10mA or less.



ELECTRICAL CHARACTERISTICS: $V_S = AV_{DD} = DV_{DD} = +5V$

			PC	SA112, PGA	113	
PARAMETER		CONDITIONS	MIN	TYP	MAX	UNIT
OFFSET VOLTAGE						
Input Offset Voltage	V _{os}	$AV_DD = DV_DD = +5V, V_REF = V_IN = AV_DD/2, V_CM = 2.5V$		±25	±100	μV
		$AV_{DD} = DV_{DD} = +5V$, $V_{REF} = V_{IN} = AV_{DD}/2$, $V_{CM} = 4.5V$		±75	±325	μV
vs Temperature, -40°C to +125°C	dV _{os} /dT	$AV_{DD} = DV_{DD} = +5V, V_{CM} = 2.5V$		0.35	1.2	μ ۷/°C
vs Temperature, -40°C to +85°C		$AV_{DD} = DV_{DD} = +5V, V_{CM} = 2.5V$		0.15	0.9	μV/°C
vs Temperature, -40°C to +125°C		$AV_{DD} = DV_{DD} = +5V, V_{CM} = 4.5V$		0.6	1.8	μ ۷/°C
vs Temperature, -40°C to +85°C		$AV_{DD} = DV_{DD} = +5V, V_{CM} = 4.5V$		0.3	1.3	μV/°C
vs Power Supply	PSRR	$AV_{DD} = DV_{DD} = +2.2V \text{ to } +5.5V, V_{CM} = 0.5V,$ $V_{REF} = V_{IN} = AV_{DD}/2$		5	20	μV/V
Over Temperature, -40°C to +125°C		$AV_{DD} = DV_{DD} = +2.2V$ to $+5.5V$, $V_{CM} = 0.5V$, $V_{REF} = V_{IN} = AV_{DD}/2$		5	40	μ V/V
INPUT ON-CHANNEL CURRENT						
Input On-Channel Current (Ch0, Ch1)	I _{IN}	$V_{REF} = V_{IN} = AV_{DD}/2$		±1.5	±5	nA
Over Temperature, -40°C to +125°C		$V_{REF} = V_{IN} = AV_{DD}/2$	See Ty	oical Charac	teristics	nA
INPUT VOLTAGE RANGE						
Input Voltage Range ⁽¹⁾	I_{VR}		GND - 0.1		AV _{DD} + 0.1	V
Overvoltage Input Range		No Output Phase Reversal (2)	GND - 0.3		$AV_{DD} + 0.3$	V
INPUT IMPEDANCE (Channel On)(3)						
Channel Input Capacitance	C _{CH}			2		pF
Channel Switch Resistance	R _{sw}			150		Ω
Amplifier Input Capacitance	C_{AMP}			3		pF
Amplifier Input Resistance	R _{AMP}	Input Resistance to GND		10		GΩ
V _{CAL} /CH0	R _{IN}	CAL1 or CAL2 Selected		100		kΩ
GAIN SELECTIONS						
Nominal Gains		Binary gains: 1, 2, 4, 8, 16, 32, 64, 128	1		128	
		Scope gains: 1, 2, 5, 10, 20, 50, 100, 200	1		200	
DC Gain Error	G = 1	$V_{OUT} = GND + 85mV$ to $DV_{DD} - 85mV$		0.006	0.1	%
	1 < G ≤ 32	$V_{OUT} = GND + 85mV$ to $DV_{DD} - 85mV$			0.1	%
	G ≥ 50	$V_{OUT} = GND + 85mV \text{ to } DV_{DD} - 85mV$			0.3	%
DC Gain Drift	G = 1	$V_{OUT} = GND + 85mV$ to $DV_{DD} - 85mV$		0.5		ppm/°C
	1 < G ≤ 32	$V_{OUT} = GND + 85mV$ to $DV_{DD} - 85mV$		2		ppm/°C
	G ≥ 50	$V_{OUT} = GND + 85mV$ to $DV_{DD} - 85mV$		6		ppm/°C
CAL2 DC Gain Error ⁽⁴⁾		Op Amp + Input = $0.9V_{CAL}$, $V_{REF} = V_{CAL} = AV_{DD}/2$, G = 1		0.02		%
CAL2 DC Gain Drift ⁽⁴⁾		Op Amp + Input = $0.9V_{CAL}$, $V_{REF} = V_{CAL} = AV_{DD}/2$, G = 1		2		ppm/°C
CAL3 DC Gain Error ⁽⁴⁾		Op Amp + Input = $0.1V_{CAL}$, $V_{REF} = V_{CAL} = AV_{DD}/2$, G = 1		0.02		%
CAL3 DC Gain Drift ⁽⁴⁾		Op Amp + Input = $0.1V_{CAL}$, $V_{REF} = V_{CAL} = AV_{DD}/2$, G = 1		2		ppm/°C
INPUT IMPEDANCE (Channel Off)(3)						
Input Impedance	С _{СН}	See Figure 1		2		pF
INPUT OFF-CHANNEL CURRENT						
Input Off-Channel Current (Ch0, Ch1) ⁽⁵⁾	I_{LKG}	$V_{REF} = GND$, $V_{OFF-CHANNEL} = AV_{DD}/2$, $V_{ON-CHANNEL} = AV_{DD}/2 - 0.1V$		±0.05	±1	nA
Over Temperature, -40°C to +125°C		V_{REF} = GND, $V_{OFF-CHANNEL}$ = $AV_{DD}/2$, $V_{ON-CHANNEL}$ = $AV_{DD}/2 - 0.1V$	See Typ			
Channel-to-Channel Crosstalk				130		dB

⁽¹⁾ Gain error is a function of the input voltage. Gain error outside of the range (GND + $85mV \le V_{OUT} \le DV_{DD} - 85mV$) increases to 0.5% (typical).

Input voltages beyond this range must be current limited to < |10mA| through the input protection diodes on each channel to prevent permanent destruction of the device. See Figure 1.

Total V_{OUT} error must be computed using input offset voltage error multiplied by gain. Includes op amp G = 1 error.

Maximum specification limitation limited by final test time and capability.



ELECTRICAL CHARACTERISTICS: $V_S = AV_{DD} = DV_{DD} = +5V$ (continued)

		PC	i		
PARAMETER	CONDITIONS	MIN	TYP	MAX	UNIT
OUTPUT					
Voltage Output Swing from Rail	$I_{OUT} = \pm 0.25 \text{mA}, \ AV_{DD} \ge DV_{DD}^{(6)}$	GND + 0.05		$\mathrm{DV}_{\mathrm{DD}} - 0.05$	V
	$I_{OUT} = \pm 5\text{mA}, \text{ AV}_{DD} \ge \text{DV}_{DD}^{(6)}$	GND + 0.25		$\mathrm{DV}_{\mathrm{DD}} - 0.25$	V
DC Output Nonlinearity	$V_{OUT} = GND + 85mV$ to $DV_{DD} - 85mV^{(7)}$		0.0015		%FSR
Short-Circuit Current I _{SC}			-30/+60		mA
Capacitive Load Drive C _{LOAD}		See Ty	pical Charact	eristics	
NOISE					
Input Voltage Noise Density e _n	$f > 10kHz, C_L = 100pF, V_S = 5V$		12		nV/√ Hz
	$f > 10kHz, C_L = 100pF, V_S = 2.2V$		22		nV/√ Hz
Input Voltage Noise e _n	$f = 0.1Hz$ to 10Hz, $C_L = 100pF$, $V_S = 5V$		0.362		μV_{PP}
	$f = 0.1Hz$ to 10Hz, $C_L = 100pF$, $V_S = 2.2V$		0.736		μV_{PP}
Input Current Density In	$f = 10kHz, C_L = 100pF$		400		fA/√ Hz
SLEW RATE					
Slew Rate SR			See Table 1		V/μs
SETTLING TIME					
Settling Time t _S			See Table 1		μs
FREQUENCY RESPONSE					,
Frequency Response			See Table 1		MHz
THD + NOISE					
	$G = 1$, $f = 1kHz$, $V_{OUT} = 4V_{PP}$ at $2.5V_{DC}$, $C_L = 100pF$		0.003		%
	$G = 10, f = 1 \text{kHz}, V_{OUT} = 4 V_{PP} \text{ at } 2.5 V_{DC}, C_1 = 100 \text{pF}$		0.005		%
	$G = 50$, $f = 1$ kHz, $V_{OUT} = 4V_{PP}$ at 2.5 V_{DC} , $C_L = 100$ pF		0.03		%
	$G = 128$, $f = 1$ kHz, $V_{OUT} = 4V_{PP}$ at 2.5 V_{DC} , $C_L = 100$ pF		0.08		%
	$G = 200$, $f = 1$ kHz, $V_{OUT} = 4V_{PP}$ at 2.5 V_{DC} , $C_1 = 100$ pF		0.1		%
	$G = 1, f = 20kHz, V_{OUT} = 4V_{PP}$ at 2.5 V_{DC} , $C_L = 100pF$		0.02		%
	$G = 10$, $f = 20$ kHz, $V_{OUT} = 4V_{PP}$ at 2.5 V_{DC} , $C_1 = 100$ pF		0.01		%
	$G = 50$, $f = 20$ kHz, $V_{OUT} = 4V_{PP}$ at $2.5V_{DC}$, $C_L = 100$ pF		0.03		%
	$G = 128$, $f = 20$ kHz, $V_{OUT} = 4V_{PP}$ at 2.5 V_{DC} , $C_L = 100$ pF		0.08		%
	$G = 200, f = 20kHz, V_{OUT} = 4V_{PP}$ at 2.5V _{DC} , $G_L = 100pF$		0.11		%
POWER SUPPLY	G = 200, I = 20kHz, V _{OUT} = 4V _{PP} at 2.5V _{DC} , C _L = 100PF		0.11		70
Operating Voltage Range ⁽⁶⁾ AV _{DD}		2.2		5.5	V
DV _{DD}		2.2		5.5	V
	$I_{O} = 0, G = 1, V_{OUT} = V_{REF}$	2.2	0.33	0.45	mA
• • • • • • • • • • • • • • • • • • • •	$i_0 = 0$, $G = 1$, $v_{OUT} = v_{REF}$		0.33	0.45	mA
Over Temperature, -40°C to +125°C	L O.C. 4 V V COLK at 40MHz			0.45	mA
Quiescent Current Digital ⁽⁸⁾⁽⁹⁾⁽¹⁰⁾ I _{QD}	I_{O} = 0, G = 1, V_{OUT} = V_{REF} , SCLK at 10MHz, \overline{CS} = Logic 0, DIO = Logic 0		0.75	1.2	mA
Over Temperature, -40°C to +125°C ⁽⁸⁾⁽⁹⁾⁽¹⁰⁾	$I_O = 0$, $G = 1$, $V_{OUT} = V_{REF}$, SCLK at 10MHz, $\overline{CS} = Logic 0$, DIO = Logic 0			1.2	mA
Shutdown Current Analog + Digital $^{(8)(9)}$ $I_{SDA} + I_{SDD}$	$I_O = 0$, $V_{OUT} = V_{REF}$, $G = 1$, SCLK Idle		4		μΑ
	$I_O = 0$, $V_{OUT} = 0$, $G = 1$, SCLK at 10MHz, $\overline{CS} = \text{Logic } 0$, DIO = Logic 0		245		μА
POWER-ON RESET (POR)	2 1 2				
POR Trip Voltage	Digital interface disabled and Command Register set to POR values for DV _{DD} < POR Trip Voltage		1.6		V

When ${\rm AV_{DD}}$ is less than ${\rm DV_{DD}}$, the output is clamped to ${\rm AV_{DD}}$ + 300mV. Measurement limited by noise in test equipment and test time.

⁽⁷⁾

 ⁽⁸⁾ Does not include current into or out of the V_{REF} pin. Internal R_F and R_I are always connected between V_{OUT} and V_{REF}.
 (9) Digital logic levels: DIO = logic 0. 10μA internal current source.

⁽¹⁰⁾ Includes current from op amp output structure.



ELECTRICAL CHARACTERISTICS: $V_s = AV_{DD} = DV_{DD} = +5V$ (continued)

		PG	6A112, PGA	113	
PARAMETER	CONDITIONS	MIN	TYP	MAX	UNIT
TEMPERATURE RANGE					
Specified Range		-40		+125	°C
Operating Range		-40		+125	°C
Thermal Resistance θ_{JA}					
MSOP-10			164		°C/W
DIGITAL INPUTS (SCLK, CS, DIO)					
Logic Low		0		0.3DV _{DD}	V
Input Leakage Current (SCLK and CS only)		-1		+1	μΑ
Weak Pull-Down Current (DIO only)			10		μΑ
Logic High		0.7DV _{DD}		DV_DD	V
Hysteresis			700		mV
DIGITAL OUTPUT (DIO)					
Logic High	$I_{OH} = -3mA$ (sourcing)	$DV_{DD} - 0.4$		DV_DD	V
Logic Low	I _{OL} = +3mA (sinking)	GND		GND + 0.4	V
CHANNEL AND GAIN TIMING					
Channel Select Time			0.2		μs
Gain Select Time			0.2		μs
SHUTDOWN MODE TIMING					
Enable Time			4.0		μs
Disable Time	V_{OUT} goes high-impedance, R_{F} and R_{I} remain connected between V_{OUT} and V_{REF}		2.0		μs
POWER-ON-RESET (POR) TIMING					
POR Power-Up Time	$DV_{DD} \ge 2V$		40		μs
POR Power-Down Time	DV _{DD} ≤ 1.5V		5		μs

Table 1. Frequency Response versus Gain ($C_L = 100 pF$, $R_L = 10 k\Omega$)

BINARY GAIN (V/V)	TYPICAL -3dB FREQUENCY (MHz)	SLEW RATE- FALL (V/μs)	SLEW RATE- RISE (V/μs)	0.1% SETTLING TIME: 4V _{PP} (μs)	0.01% SETTLING TIME: 4V _{PP} (μs)	SCOPE GAIN (V/V)	TYPICAL -3dB FREQUENCY (MHz)	SLEW RATE- FALL (V/μs)	SLEW RATE- RISE (V/µs)	0.1% SETTLING TIME: 4V _{PP} (μs)	0.01% SETTLING TIME: 4V _{PP} (μs)
1	10	8	3	2	2.55	1	10	8	3	2	2.55
2	3.8	9	6.4	2	2.6	2	3.8	9	6.4	2	2.6
4	2	12.8	10.6	2	2.6	5	1.8	12.8	10.6	2	2.6
8	1.8	12.8	10.6	2	2.6	10	1.8	12.8	10.6	2.2	2.6
16	1.6	12.8	12.8	2.3	2.6	20	1.3	12.8	9.1	2.3	2.8
32	1.8	12.8	13.3	2.3	3	50	0.9	9.1	7.1	2.4	3.8
64	0.6	4	3.5	3	6	100	0.38	4	3.5	4.4	7
128	0.35	2.5	2.5	4.8	8	200	0.23	2.3	2	6.9	10

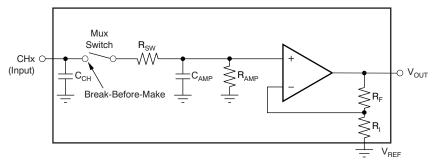


Figure 1. Equivalent Input Circuit



SPI TIMING: $V_S = AV_{DD} = DV_{DD} = +2.2V$ to +5V

				113, 117		
PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
Input Capacitance (SCLK, CS, and DIO pins)				1		pF
Input Rise/Fall Time ⁽¹⁾ (CS, SCLK, and DIO pins)	t _{RFI}				2	μs
Output Rise/Fall Time (DIO pin) ⁽¹⁾	t _{RFO}	$C_{LOAD} = 60pF$			10	ns
CS High Time (CS pin) ⁽¹⁾	t _{CSH}		40			ns
SCLK Edge to CS Fall Setup Time(1)	t_{CSO}		10			ns
CS Fall to First SCLK Edge Setup Time	t _{CSSC}		10			ns
SCLK Frequency ⁽²⁾	f _{SCLK}				10	MHz
SCLK High Time ⁽³⁾	t _{HI}		40			ns
SCLK Low Time ⁽³⁾	t_{LO}		40			ns
SCLK Last Edge to CS Rise Setup Time (1)	t _{SCCS}		10			ns
CS Rise to SCLK Edge Setup Time (1)	t _{CS1}		10			ns
DIN Setup Time	t _{SU}		10			ns
DIN Hold Time	t_{HD}		10			ns
SCLK to DOUT Valid Propagation Delay ⁽¹⁾	t_{DO}				25	ns
CS Rise to DOUT Forced to Hi-Z ⁽¹⁾	t _{SOZ}				20	ns

⁽¹⁾ Ensured by design; not production tested.

When using devices in daisy-chain mode, the maximum clock frequency for SCLK is determined by a combination of propagation delay time ($t_{DO} \le 25$ ns), data input setup time ($t_{SU} \ge 10$ ns), SCLK high time ($t_{HI} \ge 40$ ns), and DOUT rise and fall times ($t_{RFO} \le 10$ ns). In addition, maximum clock frequency depends directly on the number of devices in the daisy-chain.

⁽³⁾ t_{HI} and t_{LO} must not be less than 1/SCLK (max).



SPI TIMING DIAGRAMS

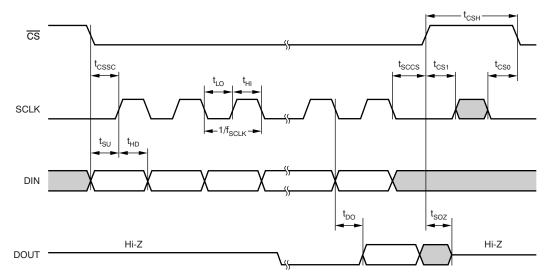


Figure 2. SPI Mode 0, 0

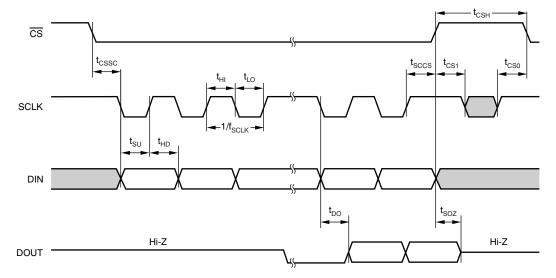
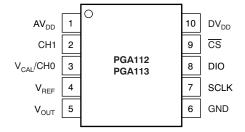


Figure 3. SPI Mode 1, 1



PIN CONFIGURATIONS

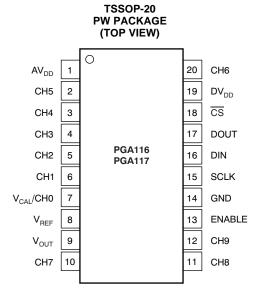
MSOP-10 DGS PACKAGE (TOP VIEW)



PGA112, PGA113 TERMINAL FUNCTIONS

MSOP PACKAGE PIN #	NAME	DESCRIPTION						
1	AV _{DD}	Analog supply voltage (+2.2V to +5.5V)						
2	CH1	Input MUX channel 1						
3	V _{CAL} /CH0	Input MUX channel 0 and V_{CAL} input. For system calibration purposes, connect this pin to a low-impedance external reference voltage to use internal calibration channels. The four internal calibration channels are connected to GND, $0.9V_{CAL}$, $0.1V_{CAL}$, and V_{REF} , respectively. V_{CAL} is loaded with $100k\Omega$ (typical) when internal calibration channels CAL2 or CAL3 are selected. Otherwise, $V_{CAL}/CH0$ appears as high impedance.						
4	V _{REF}	Reference input pin. Connect external reference for V_{OUT} offset shift or to midsupply for midsupply referenced systems. V_{REF} must be connected to a low-impedance reference capable of sourcing and sinking at least 2mA or V_{REF} must be connected to GND.						
5	V _{OUT}	Analog voltage output. When $AV_{DD} < DV_{DD}$, V_{OUT} is clamped to $AV_{DD} + 300$ mV.						
6	GND	Ground pin						
7	SCLK	Clock input for SPI serial interface						
8	DIO	Data input/output for SPI serial interface. DIO contains a weak, 10µA internal pull-down current source.						
9	<u>CS</u>	Chip select line for SPI serial interface						
10	DV _{DD}	Digital and op amp output stage supply voltage ($\pm 2.2V$ to $\pm 5.5V$). Useful in multi-supply systems to prevent overvoltage/lockup condition on an analog-to-digital (ADC) input (for example, a microcontroller with an ADC running on $\pm 3V$ and the PGA powered from $\pm 5V$). Digital I/O levels to be relative to DV_{DD} . DV_{DD} should be bypassed with a $0.1\mu F$ ceramic capacitor, and DV_{DD} must supply the current for the digital portion of the PGA as well as the load current for the op amp output stage.						





PGA116, PGA117 TERMINAL FUNCTIONS

TSSOP PACKAGE PIN #	NAME	DESCRIPTION
1	AV_{DD}	Analog supply voltage (+2.2V to +5.5V)
2	CH5	Input MUX channel 5
3	CH4	Input MUX channel 4
4	CH3	Input MUX channel 3
5	CH2	Input MUX channel 2
6	CH1	Input MUX channel 1
7	V _{CAL} /CH0	Input MUX channel 0 and V_{CAL} input. For system calibration purposes, connect this pin to a low-impedance external reference voltage to use internal calibration channels. The four internal calibration channels are connected to GND, $0.9V_{CAL}$, $0.1V_{CAL}$, and V_{REF} , respectively. V_{CAL} is loaded with $100k\Omega$ (typical) when internal calibration channels CAL2 or CAL3 are selected. Otherwise, $V_{CAL}/CH0$ appears as high impedance.
8	V _{REF}	Reference input pin. Connect external reference for V_{OUT} offset shift or to midsupply for midsupply referenced systems. V_{REF} must be connected to a low-impedance reference capable of sourcing and sinking at least 2mA or to GND.
9	V _{OUT}	Analog voltage output. When $AV_{DD} < DV_{DD}$, V_{OUT} is clamped to $AV_{DD} + 300$ mV.
10	CH7	Input MUX channel 7
11	CH8	Input MUX channel 8
12	CH9	Input MUX channel 9
13	ENABLE	Hardware enable pin. Logic low puts the part into Shutdown mode (I_Q < 1 μ A).
14	GND	Ground pin
15	SCLK	Clock input for SPI serial interface
16	DIN	Data input for SPI serial interface. DIN contains a weak, 10µA internal pull-down current source to allow for ease of daisy-chain configurations.
17	DOUT	Data output for SPI serial interface. DOUT goes to high-Z state when $\overline{\text{CS}}$ goes high for standard SPI interface.
18	CS	Chip select line for SPI serial interface
19	DV _{DD}	Digital and op amp output stage supply voltage (+2.2V to +5.5V). Useful in multi-supply systems to prevent overvoltage/lockup condition on an ADC input (for example, a microcontroller with an ADC running on +3V and the PGA powered from +5V). Digital I/O levels to be relative to DV _{DD} . DV _{DD} should be bypassed with a $0.1\mu F$ ceramic capacitor, and DV _{DD} must supply the current for the digital portion of the PGA as well as the load current for the op amp output stage.
20	CH6	Input MUX channel 6



TYPICAL APPLICATION CIRCUITS

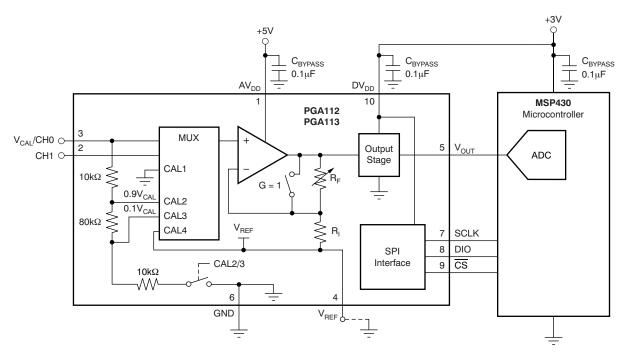


Figure 4. PGA112, PGA113 (MSOP-10)

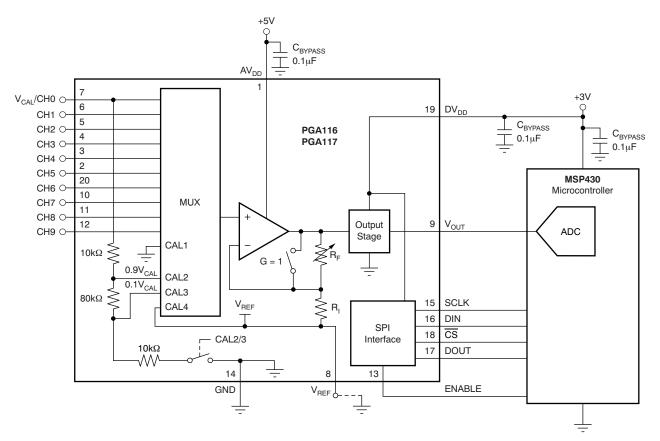


Figure 5. PGA116, PGA117 (TSSOP-20)



TYPICAL CHARACTERISTICS

At $T_A = +25$ °C, $AV_{DD} = DV_{DD} = 5V$, $R_L = 10k\Omega$ connected to $DV_{DD}/2$, $V_{REF} = GND$, and $C_L = 100pF$, unless otherwise noted.

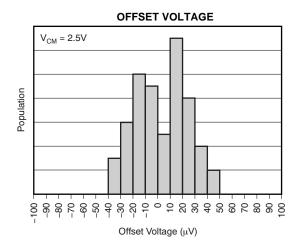


Figure 6.

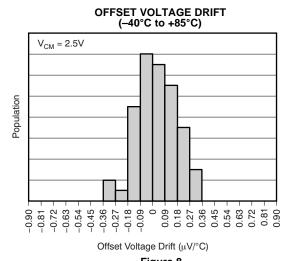


Figure 8.

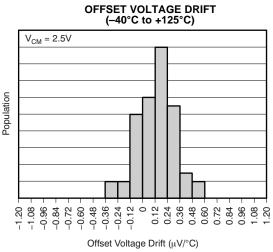


Figure 10.

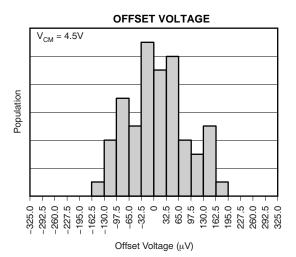
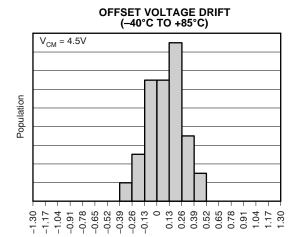


Figure 7.



Offset Voltage Drift (μ V/°C) Figure 9.

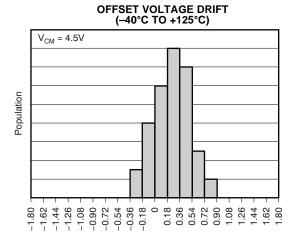


Figure 11.



At $T_A = +25^{\circ}C$, $AV_{DD} = DV_{DD} = 5V$, $R_L = 10k\Omega$ connected to $DV_{DD}/2$, $V_{REF} = GND$, and $C_L = 100pF$, unless otherwise noted.

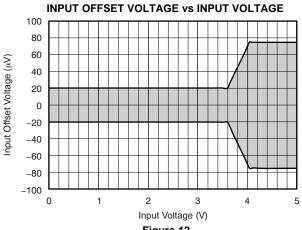


Figure 12.

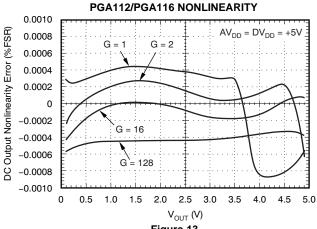


Figure 13.

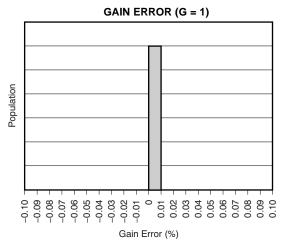


Figure 14.

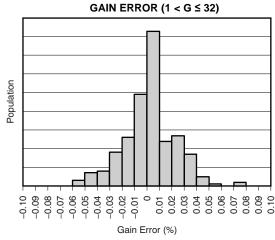
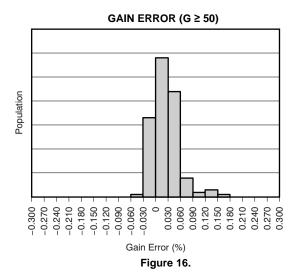


Figure 15.

GAIN ERROR DRIFT (-40°C to +125°C)



G = 1

Gain Error Drift (ppm/°C)

Population



At $T_A = +25^{\circ}C$, $AV_{DD} = DV_{DD} = 5V$, $R_L = 10k\Omega$ connected to $DV_{DD}/2$, $V_{REF} = GND$, and $C_L = 100pF$, unless otherwise noted.

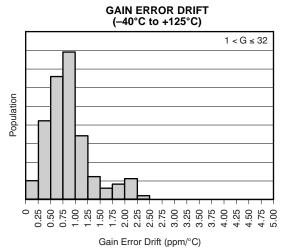


Figure 18.

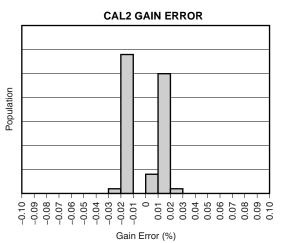
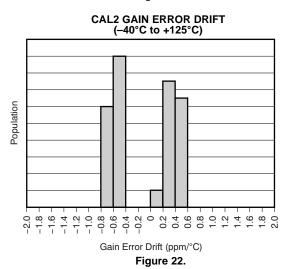


Figure 20.



GAIN ERROR DRIFT (-40°C to +125°C)

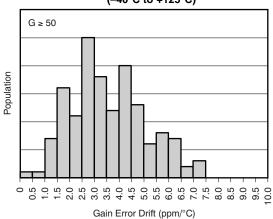


Figure 19.



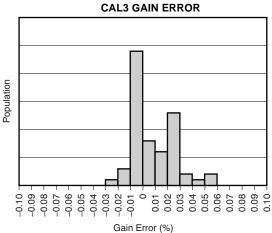


Figure 21.

CAL3 GAIN ERROR DRIFT (-40°C to +125°C)

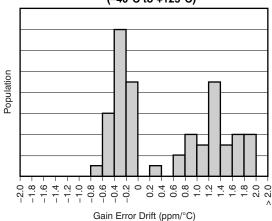
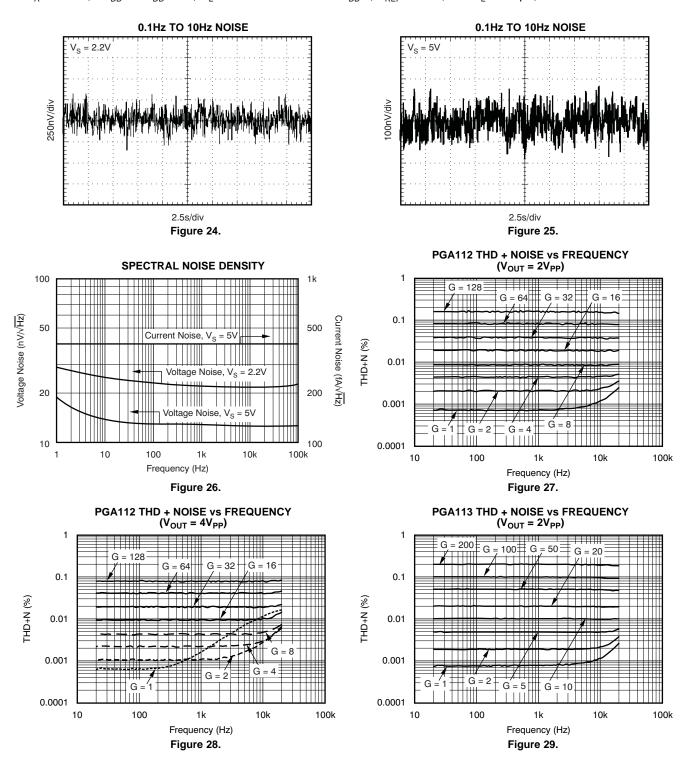


Figure 23.

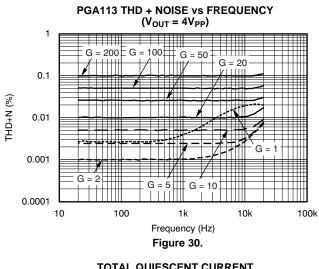


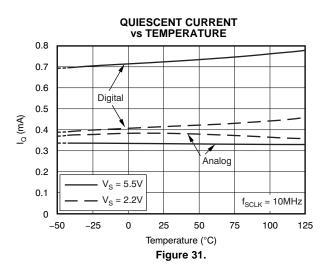
At $T_A = +25^{\circ}C$, $AV_{DD} = DV_{DD} = 5V$, $R_L = 10k\Omega$ connected to $DV_{DD}/2$, $V_{REF} = GND$, and $C_L = 100pF$, unless otherwise noted.

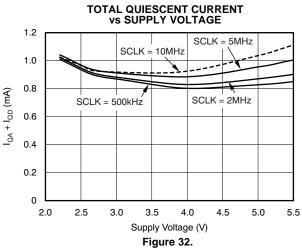


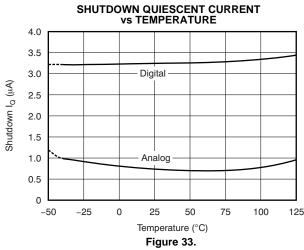


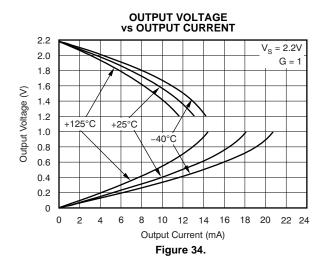
At $T_A = +25^{\circ}C$, $AV_{DD} = DV_{DD} = 5V$, $R_L = 10k\Omega$ connected to $DV_{DD}/2$, $V_{REF} = GND$, and $C_L = 100pF$, unless otherwise noted.

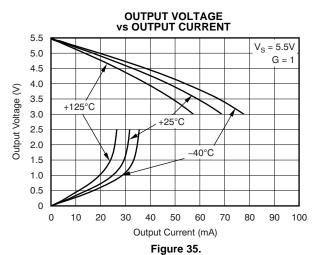






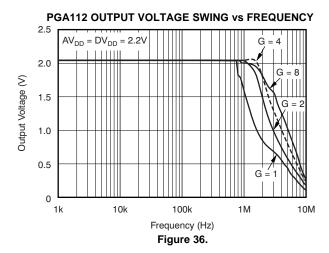


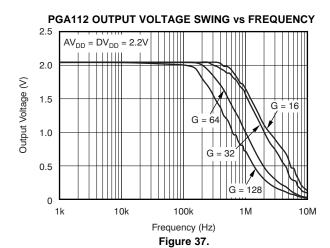


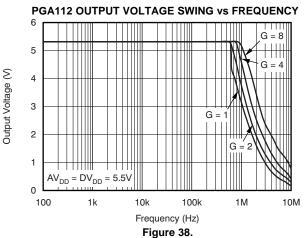


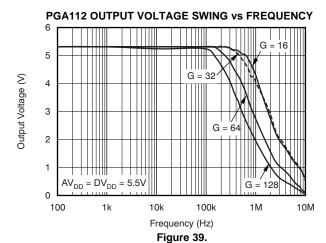


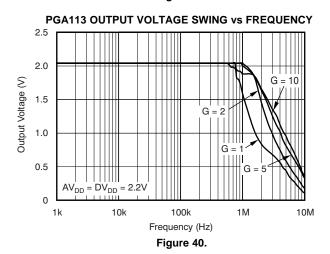
At $T_A = +25$ °C, $AV_{DD} = DV_{DD} = 5V$, $R_L = 10k\Omega$ connected to $DV_{DD}/2$, $V_{REF} = GND$, and $C_L = 100pF$, unless otherwise noted.

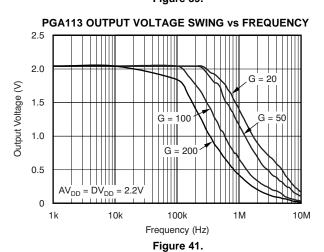






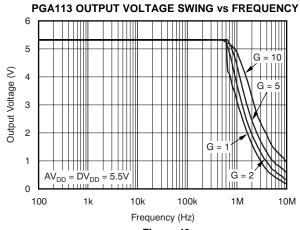








At $T_A = +25$ °C, $AV_{DD} = DV_{DD} = 5V$, $R_L = 10k\Omega$ connected to $DV_{DD}/2$, $V_{REF} = GND$, and $C_L = 100pF$, unless otherwise noted.





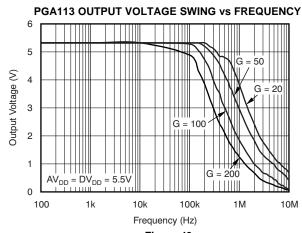
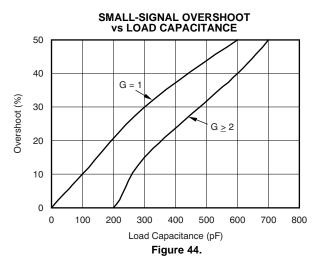
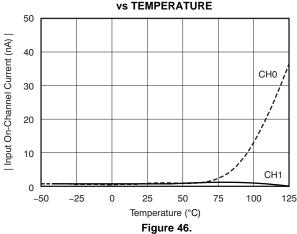


Figure 43.



INPUT ON-CHANNEL CURRENT **VS TEMPERATURE**



GAIN vs SETTLING TIME

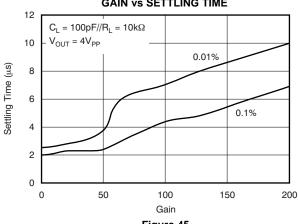


Figure 45.



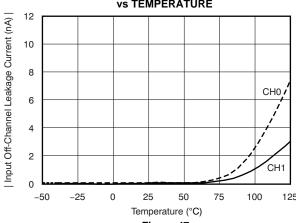
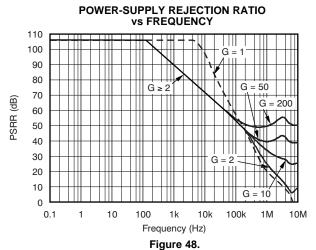
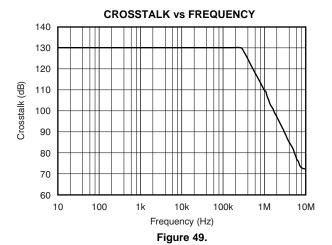


Figure 47.

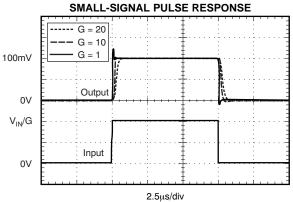


At $T_A = +25^{\circ}C$, $AV_{DD} = DV_{DD} = 5V$, $R_L = 10k\Omega$ connected to $DV_{DD}/2$, $V_{REF} = GND$, and $C_L = 100pF$, unless otherwise noted.









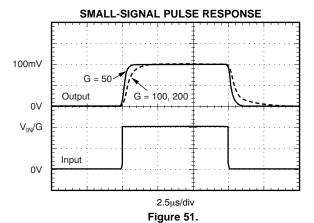
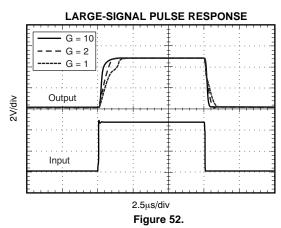


Figure 50.



LARGE-SIGNAL PULSE RESPONSE

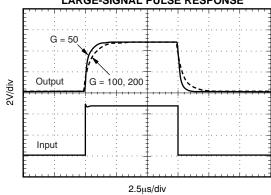
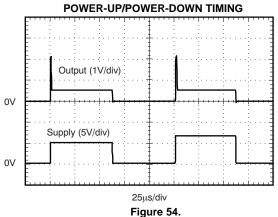


Figure 53.



At $T_A = +25$ °C, $AV_{DD} = DV_{DD} = 5V$, $R_L = 10k\Omega$ connected to $DV_{DD}/2$, $V_{REF} = GND$, and $C_L = 100pF$, unless otherwise noted.



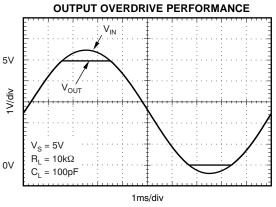
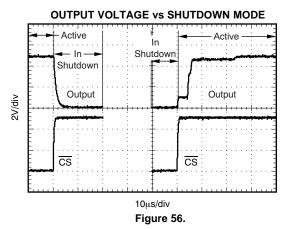


Figure 55.



SERIAL INTERFACE INFORMATION

SERIAL DIGITAL INTERFACE: SPI MODES

The PGA uses a standard serial peripheral interface (SPI). Both SPI Mode 0,0 and Mode 1,1 are supported, as shown in Figure 57 and described in Table 2.

If there are not even-numbered increments of $\frac{16}{CS}$ clocks (that is, 16, 32, 64, and $\frac{so}{CS}$ forth) between $\frac{16}{CS}$ going low (falling edge) and $\frac{16}{CS}$ going high (rising

edge), the device takes no action. This condition provides reliable serial communication. Furthermore, this condition also provides a way to quickly reset the SPI interface to a known starting condition for data synchronization. Transmitted data are latched internally on the rising edge of CS.



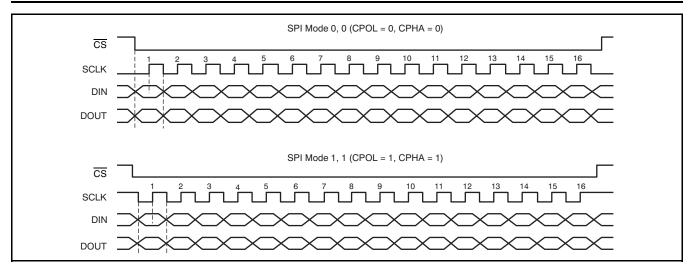


Figure 57. SPI Mode 0,0 and Mode 1,1

Table 2. SPI Mode Setting Description

N	MODE	CPOL	СРНА	CPOL DESCRIPTION	CPHA DESCRIPTION							
	0, 0	0	0 ⁽¹⁾	Clock idles low	Data are read on the rising edge of clock. Data change on the falling edge of clock.							
	1, 1	1	1 (2)	Clock idles high	Data are read on the rising edge of clock. Data change on the falling edge of clock.							

(1) CPHA = 0 means sample on first clock edge (rising or falling) after a valid (S).
 (2) CPHA = 1 means sample on second clock edge (rising or falling) after a valid (S).

On the PGA116/PGA117, $\overline{\text{CS}}$, DIN, and SCLK are Schmitt-triggered CMOS logic inputs. DIN has a weak internal pull-down to support daisy-chain communications on the PGA116/PGA117. DOUT is a CMOS logic output. When $\overline{\text{CS}}$ is high, the state of DOUT is high-impedance. When $\overline{\text{CS}}$ is low, DOUT is driven as illustrated in Figure 58.

On the PGA112/PGA113, there are digital output and digital input gates both internally connected to the DIO pin. DIN is an input-only gate and DOUT is a digital output that can give a 3-state output. The DIO pin has a weak 10µA pull-down current source to prevent the pin from floating in systems with a high-impedance SPI DOUT line. When \overline{CS} is high, the state of the internal DOUT gate is high-impedance. When \overline{CS} is low, the state of DIO depends on the previous valid SPI communication; either DIO becomes an output to clock out data or it remains an input to receive data. This structure is shown in Figure 59.

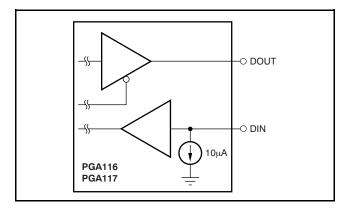


Figure 58. Digital I/O Structure—PGA116/PGA117

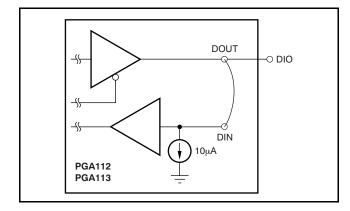


Figure 59. Digital I/O Structure—PGA112/PGA113



SPI SERIAL INTERFACE: PGA112/PGA113 ONLY

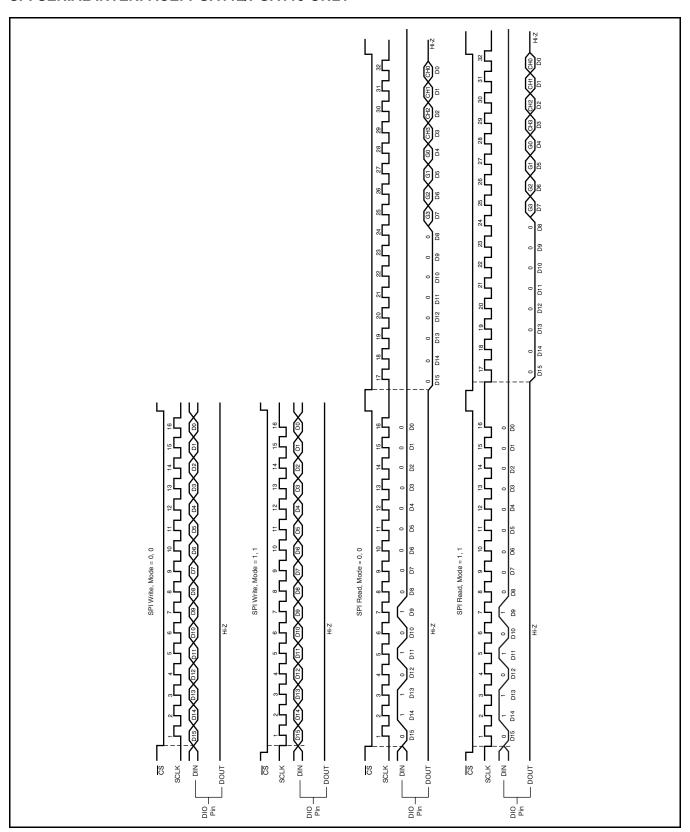


Figure 60. SPI Serial Interface Timing Diagrams



SPI COMMANDS: PGA112/PGA113 ONLY

Table 3. SPI Commands (PGA112/PGA113)(1)(2)

D15	D14	D13	D12	D11	D10	D9	D8	D7	D6	D5	D4	D3	D2	D1	D0	THREE-WIRE SPI COMMAND
0	1	1	0	1	0	1	0	0	0	0	0	0	0	0	0	READ
0	0	1	0	1	0	1	0	G3	G2	G1	G0	CH3	CH2	CH1	CH0	WRITE
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	NOP WRITE
1	1	1	0	0	0	0	1	0	0	0	0	0	0	0	0	SDN_DIS WRITE
1	1	1	0	0	0	0	1	1	1	1	1	0	0	0	1	SDN_EN WRITE

⁽¹⁾ SDN = Shutdown mode. Enter Shutdown mode by issuing an SDN_EN command. Shutdown mode is cleared (returned to the last valid write configuration) by a SDN_DIS command or by any valid Write command.

Table 4. Gain Selection Bits (PGA112/PGA113)

G3	G2	G1	G0	BINARY GAIN	SCOPE GAIN
0	0	0	0	1	1
0	0	0	1	2	2
0	0	1	0	4	5
0	0	1	1	8	10
0	1	0	0	16	20
0	1	0	1	32	50
0	1	1	0	64	100
0	1	1	1	128	200

Table 5. MUX Channel Selection Bits (PGA112/PGA113)

СНЗ	CH2	CH1	СНО	PGA112 PGA113
0	0	0	0	V _{CAL} /CH0
0	0	0	1	CH1
0	0	1	0	X ⁽¹⁾
0	0	1	1	X
0	1	0	0	X
0	1	0	1	X
0	1	1	0	X
0	1	1	1	X
1	0	0	0	X
1	0	0	1	X
1	0	1	0	Factory Reserved
1	0	1	1	X
1	1	0	0	CAL1 ⁽²⁾
1	1	0	1	CAL2 ⁽³⁾
1	1	1	0	CAL3 ⁽⁴⁾
1	1	1	1	CAL4 ⁽⁵⁾

(1) X = channel is not used.

(2) CAL1: connects to GND.

(3) CAL2: connects to 0.9V_{CAL}.

(4) CAL3: connects to 0.1V_{CAL}.

(5) CAL4: connects to V_{REF} .

⁽²⁾ POR (power-on-reset) value of internal Gain/Channel Select Register is all 0s. This value sets Gain = 1, and Channel = V_{CAL}/CH0.



APPLICATION INFORMATION

FUNCTIONAL DESCRIPTION

The PGA112/PGA113 and PGA116/PGA117 are single-ended input, single-supply, programmable gain amplifiers with an input multiplexer. Multiplexer channel selection and gain selection are done through standard SPI interface. PGA112/PGA113 have a two-channel input MUX and the PGA116/PGA117 have a 10-channel input MUX. The PGA112 and PGA116 provide binary gain selections (1, 2, 4, 8, 16, 32, 64, 128) and the PGA113 and PGA117 provide scope gain selections (1, 2, 5, 10, 20, 50, 100, 200). All models use a split-supply architecture with an analog supply, AV_{DD}, and a digital supply, DV_{DD} . This split-supply architecture allows for ease of interface to analog-to-digital (ADCs) converters and microcontrollers in mixed-supply voltage systems, such as where the analog supply is +5V and the digital supply is +3V. Four internal calibration channels are provided for system-level calibration. The channels are tied to GND, 0.9V_{CAL}, 0.1V_{CAL}, and V_{REF} , respectively. V_{CAL} , an external voltage connected to $V_{CAL}/CH0$, acts as the system calibration reference. If V_{CAL} is the system ADC reference, then gain and offset calibration on the ADC are easily accomplished through the PGA using only one MUX input. If calibration is not used, then V_{CAI}/CH0 can be used as a standard MUX input. All four versions provide a V_{RFF} pin that can be tied to ground or, for ease of scaling, to midsupply in single-supply systems where midsupply is used as a virtual ground. The PGA112/PGA113 offer a software-controlled shutdown feature for low standby power. The PGA116/PGA117 offer both hardwareand software-controlled shutdown for low standby power. The PGA112/PGA113 have a three-wire SPI digital interface; the PGA116/PGA117 have a four-wire SPI digital interface. The PGA116/117 also have daisy-chain capability.

OP AMP: INPUT STAGE

The PGA op amp is a rail-to-rail input and output (RRIO) single-supply op amp. The input topology uses two separate input stages in parallel to achieve rail-to-rail input. As Figure 61 shows, there is a PMOS transistor on each input for operation down to ground; there is also an NMOS transistor on each input in parallel for operation to the positive supply rail. When the common-mode input voltage (that is, the single-ended input, because this PGA is configured internally for noninverting gain) crosses a level that is typically about 1.5V below the positive supply, there is a transition between the NMOS and

PMOS transistors. The result of this transition appears as a small input offset voltage transition that is reflected to the output by the selected PGA gain. This transition may be either increasing or decreasing, and differs from part to part as described in Figure 62 and Figure 63. These figures illustrate possible differences in input offset voltage between two different devices when used with ${\rm AV_{DD}} = +5{\rm V}$. Because the exact transition region varies from device to device, the Electrical Characteristics table specifies an input offset voltage above and below this input transition region.

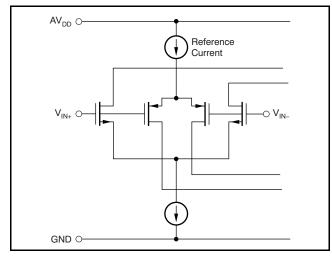


Figure 61. PGA Rail-to-Rail Input Stage

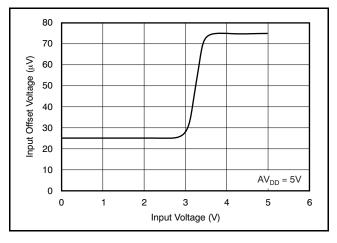


Figure 62. V_{OS} versus Input Voltage—Case 1



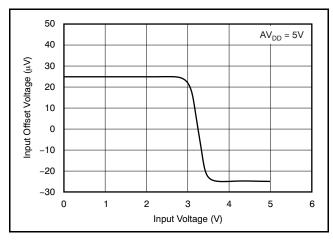


Figure 63. Vos versus Input Voltage—Case 2

OP AMP: GENERAL GAIN EQUATIONS

Figure 64 shows the basic configuration for using the PGA112/113 as a gain block. V_{OUT}/V_{IN} is the selected noninverting gain, depending on the model selected, for either binary or scope gains.

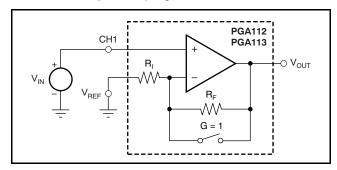


Figure 64. PGA112/PGA113 Used as a Gain Block

$$V_{OUT} = G \times V_{IN}$$
 (1)

Where:

G = 1, 2, 4, 8, 16, 32, 64, and 128 (binary gains)G = 1, 2, 5, 10, 20, 50, 100, and 200 (scope gains)

Figure 65 shows the PGA configuration and gain equations for $V_{REF} = AV_{DD}/2$. V_{OUT0} is V_{OUT} when CH0 is selected and V_{OUT1} is V_{OUT} when CH1 is selected. Notice the V_{REF} pin has no effect for G=1 because the internal feedback resistor, R_F , is shorted out. This configuration allows for positive and negative voltage excursions around a midsupply virtual ground.

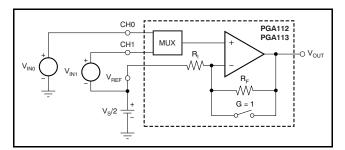


Figure 65. PGA112/PGA113 Configuration for Positive and Negative Excursions Around Midsupply Virtual Ground

$$V_{OUT0} = G \times V_{IN0} - AV_{DD}/2 \times (G - 1)$$
 (2)

When: G = 1

Then: $V_{OUT0} = G \times V_{IN0}$

$$V_{OUT1} = G \times (V_{IN1} + AV_{DD}/2) - AV_{DD}/2 \times (G - 1)$$

 $V_{OUT1} = G \times V_{IN1} + AV_{DD}/2$, where: $-AV_{DD}/2 < G \times V_{IN1} < +AV_{DD}/2$ (3)

Where:

G = 1, 2, 4, 8, 16, 32, 64, and 128 (binary gains)G = 1, 2, 5, 10, 20, 50, 100, and 200 (scope gains)

Table 6 details the internal typical values for the op amp internal feedback resistor (R_F) and op amp internal input resistor (R_I) for both binary and scope gains.

Table 6. Typical R_F and R_I versus Gain

Binary Gain (V/V)	R _F (Ω)	R _I (Ω)	Scope Gain (V/V)	R _F (Ω)	R _I (Ω)
1	0	3.25k	1	0	3.25k
2	3.25k	3.25k	2	3.25k	3.25k
4	9.75k	3.25k	5	13k	3.25k
8	22.75k	3.25k	10	29.25k	3.25k
16	48.75k	3.25k	20	61.75k	3.25k
32	100.75k	3.25k	50	159.25k	3.25k
64	204.75k	3.25k	100	321.75k	3.25k
128	412.75k	3.25k	200	646.75k	3.25k

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OP AMP: FREQUENCY RESPONSE VERSUS GAIN

Table 7 documents how small-signal bandwidth and slew rate change correspond to changes in PGA gain.

Full power bandwidth (that is, the highest frequency that a sine wave can pass through the PGA for a given gain) is related to slew rate by Equation 4:

SR
$$(V/\mu s) = 2\pi f \times V_{OP} (1 \times 10^{-6})$$
 (4)

Where:

SR = Slew rate in V/μs f = Frequency in Hz V_{OP} = Output peak voltage in volts

Example:

For G = 8, then SR = $10.6V/\mu s$ (slew rate rise is minimum slew rate).

For a 5V system, choose $0.1V < V_{OUT} < 4.9V$ or $V_{OUTP} = 4.8V$ or $V_{OUTP} = 2.4V$.

SR $(V/\mu s) = 2\pi f \times V_{OP} (1 \times 10^{-6}).$

 $10.6 = 2\pi f (2.4) (1 \times 10^{-6}) \rightarrow f = 702.9 \text{kHz}$

This example shows that a G = 8 configuration can produce a 4.8V_{PP} sine wave with frequency up to 702.9kHz. This computation only shows the theoretical upper limit of frequency for this example, but does not indicate the distortion of the sine wave. The acceptable distortion depends on the specific application. As a general guideline, maintain two to three times the calculated slew rate to minimize distortion on the sine wave. For this example, the application should only use G = 8, $4.8V_{PP}$, up to a frequency range of 234kHz to 351kHz, depending upon the acceptable distortion. For a given gain and slew rate requirement, check for adequate small-signal bandwidth (typical -3dB frequency) in order to assure that the frequency of the signal can be passed without attenuation.

ANALOG MUX

The analog input MUX provides two input channels for the PGA112/PGA113 and 10 input channels for the PGA116/PGA117. The MUX switches are designed to be break-before-make and thereby eliminate any concerns about shorting the two input signal sources together.

Four internal MUX CAL channels are included in the analog MUX for ease of system calibration. These CAL channels allow ADC gain and offset errors to be calibrated out. This calibration does not remove the offset and gain errors of the PGA for gains greater than 1, but most systems should see a significant increase in the ADC accuracy. In addition, these CAL channels can be used by the ADC to read the minimum and maximum possible voltages from the PGA. With these minimum and maximum levels known, the system architecture can be designed to indicate an out-of-range condition on the measured analog input signals if these levels are ever measured.

To use the CAL channels, $V_{CAL}/CH0$ must be permanently connected to the system ADC reference. There is a typical $100k\Omega$ load from $V_{CAL}/CH0$ to ground. Table 8 illustrates how to use the CAL channels with V_{REF} = ground. Table 9 describes how to use the CAL channels with V_{REF} = $AV_{DD}/2$. The V_{REF} pin must be connected to a source that is low-impedance for both dc and ac in order to maintain gain and nonlinearity accuracy. Worst-case current demand on the V_{REF} pin occurs when G=1 because there is a $3.25k\Omega$ resistor between V_{OUT} and V_{REF} . For a 5V system with $AV_{DD}/2=2.5V$, the V_{REF} pin buffer must source and sink $2.5V/3.25k\Omega=0.7mA$ minimum for a V_{OUT} that can swing from ground to +5V.

Table 7. Frequency Response versus Gain ($C_1 = 100 \text{pF}$, $R_1 = 10 \text{k}\Omega$)

BINARY GAIN (V/V)	TYPICAL -3dB FREQUENCY (MHz)	SLEW RATE- FALL (V/µs)	SLEW RATE- RISE (V/µs)	0.1% SETTLING TIME: 4V _{PP} (μs)	0.01% SETTLING TIME: 4V _{PP} (μs)	SCOPE GAIN (V/V)	TYPICAL -3dB FREQUENCY (MHz)	SLEW RATE- FALL (V/µs)	SLEW RATE- RISE (V/µs)	0.1% SETTLING TIME: 4V _{PP} (μs)	0.01% SETTLING TIME: 4V _{PP} (μs)
1	10	8	3	2	2.55	1	10	8	3	2	2.55
2	3.8	9	6.4	2	2.6	2	3.8	9	6.4	2	2.6
4	2	12.8	10.6	2	2.6	5	1.8	12.8	10.6	2	2.6
8	1.8	12.8	10.6	2	2.6	10	1.8	12.8	10.6	2.2	2.6
16	1.6	12.8	12.8	2.3	2.6	20	1.3	12.8	9.1	2.3	2.8
32	1.8	12.8	13.3	2.3	3	50	0.9	9.1	7.1	2.4	3.8
64	0.6	4	3.5	3	6	100	0.38	4	3.5	4.4	7
128	0.35	2.5	2.5	4.8	8	200	0.23	2.3	2	6.9	10



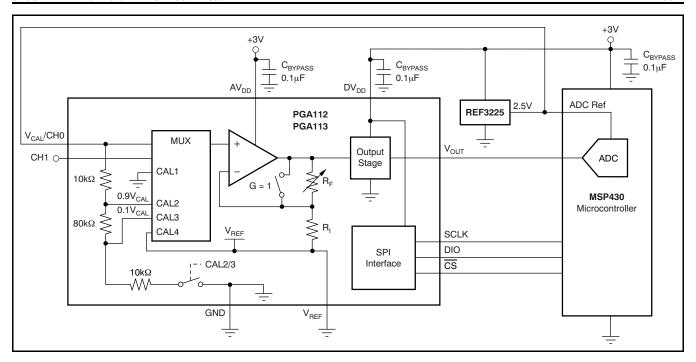


Figure 66. Using CAL Channels with V_{REF} = Ground

Table 8. Using the MUX CAL Channels with V_{REF} = GND (AV_{DD} = 3V, DV_{DD} = 3V, ADC Ref = 2.5V, and V_{REF} = GND)

FUNCTION	MUX SELECT	GAIN SELECT	MUX INPUT	OP AMP (+ln)	OP AMP (V _{OUT})	DESCRIPTION
Minimum Signal	CAL1	1	GND	GND	50mV	Minimum signal level that the MUX, op amp, and ADC can read. Op amp V _{OUT} is limited by negative saturation.
Gain Calibration	CAL2	1	0.9 × (V _{CAL} /CH0)	2.25V	2.25V	90% ADC Ref for system full-scale or gain calibration of the ADC.
Maximum Signal	CAL2	2	0.9 × (V _{CAL} /CH0)	2.25V	2.95V	Maximum signal level that the MUX, op amp, and ADC can read. Op amp V _{OUT} is limited by positive saturation. System is limited by ADC max input of 2.5V (ADC Ref = 2.5V).
Offset Calibration	CAL3	1	0.1 × (V _{CAL} /CH0)	0.25V	0.25V	10% ADC Ref for system offset calibration of the ADC.
Minimum Signal	CAL4	1	V _{REF}	GND	50mV	Minimum signal level that the MUX, op amp, and ADC can read. Op amp V _{OUT} is limited by negative saturation.



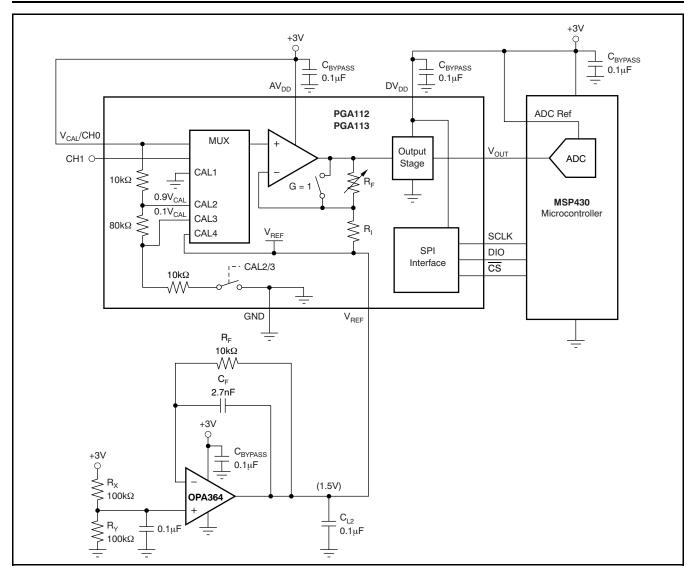


Figure 67. Using CAL Channels with $V_{REF} = AV_{DD}/2$

Table 9. Using the MUX CAL Channels with $V_{REF} = AV_{DD}/2$ (AV $_{DD} = 3V$, DV $_{DD} = 3V$, ADC Ref = 3V, and $V_{REF} = 1.5V$)

FUNCTION	MUX SELECT	GAIN SELECT	MUX INPUT	OP AMP (+ln)	OP AMP (V _{OUT})	DESCRIPTION
Minimum Signal	CAL1	1	GND	GND	50mV	Minimum signal level that the MUX, op amp, and ADC can read. Op amp V _{OUT} is limited by negative saturation.
Gain Calibration	CAL2	1	0.9 × (V _{CAL} /CH0)	2.7V	2.7V	90% ADC Ref for system full-scale or gain calibration of the ADC.
Maximum Signal	CAL2	4 or 5	0.9 × (V _{CAL} /CH0)	2.25V	2.95V	Maximum signal level that the MUX, op amp, and ADC can read. Op amp V _{OUT} is limited by positive saturation.
Offset Calibration	CAL3	1	0.1 x (V _{CAL} /CH0)	0.3V	0.3V	10% ADC Ref for system offset calibration of the ADC.
V _{REF} Check	CAL4	1	V _{REF}	1.5V	1.5V	Midsupply voltage used as V _{REF} .



SYSTEM CALIBRATION USING THE PGA112/PGA113

Analog-to-digital converters (ADCs) contain two major errors that can be easily removed by calibration at a system level. These errors are gain error and offset error, as shown in Figure 68. Figure 68 shows a typical transfer function for a 12-bit ADC. The analog input is on the x-axis with a range from 0V to $(V_{REF\ ADC}\ -\ 1LSB)$, where V_{REF_ADC} is the ADC reference voltage. The y-axis is the hexadecimal equivalent of the digital codes that result from ADC conversions. The dotted red line represents an ideal transfer function with 0000h representing 0V analog input and OFFFh representing an analog input of $(V_{REF_ADC} - 1LSB)$. The solid blue line illustrates the offset error. Although the solid blue line includes both offset error and gain error, at an analog input of 0V the offset error voltage, V_{Z ACTUAL}, can be measured. The dashed black line represents the transfer function with gain error. The dashed black line is equivalent to the solid blue line without the offset error, and can be measured and computed using V_{Z_ACTUAL} and V_{Z IDEAL}. The difference between the dashed black line and the dotted red line is the gain error. Gain and offset error can be computed by taking zero input and full-scale input readings. Using these error calculations, compute a calibrated ADC reading to remove the ADC gain and offset error.

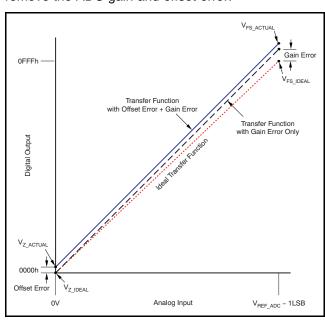


Figure 68. ADC Offset and Gain Error

In practice, the zero input (0V) or full-scale input (V_{REF ADC} - 1LSB) of ADCs cannot always be measured because of internal offset error and gain error. However, if measurements are made very close to the full-scale input and the zero input, both zero and full-scale can be calibrated very accurately with the assumption of linearity from the calibration points to the desired end points of the ADC ideal transfer function. For the zero calibration, $10\%V_{REF_ADC}$; this value should be above the internal offset error and sufficiently out of the noise floor range of the ADC. For the gain calibration, choose 90%V_{REF ADC}; this value should be less than the internal gain error and sufficiently below the tolerance of V_{REE}. These key points can be summarized in this way:

For zero calibration:

- The ADC cannot read the ideal zero because of offset error
- Must be far enough above ground to be above noise floor and ADC offset error
- Therefore, choose 10%V_{REF_ADC} for zero calibration

For gain calibration:

- The ADC cannot read the ideal full-scale because of gain error
- Must be far enough below full-scale to be below the V_{REF} tolerance and ADC gain error
- Therefore, choose 90%V_{REF_ADC} for gain calibration



The 12-bit ADC example in Figure 69 illustrates the technique for calibrating an ADC using a $10\% V_{REF_ADC}$ and $90\% V_{REF_ADC}$ reading where V_{REF_ADC} is the ADC reference voltage. Note that the $10\% V_{REF}$ reading also contains a gain error because it is not a $V_{IN}=0$ calibration point. First, use the $90\% V_{REF}$ and $10\% V_{REF}$ points to compute the measured gain error. The measured gain error is then used to remove the gain error from the $10\% V_{REF}$ reading, giving a measured $10\% V_{REF}$ number. The measured $10\% V_{REF}$ number is used to compute the measured offset error.

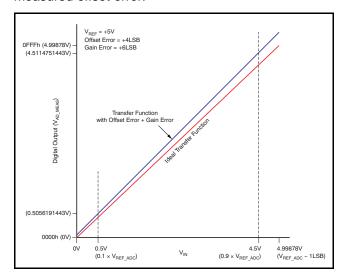


Figure 69. 12-Bit Example of ADC Calibration for Gain and Offset Error

The gain error and offset error in ADC readings can be calibrated by using 10%V $_{REF_ADC}$ and 90%V $_{REF_ADC}$ calibration points. Because the calibration is ratiometric to V $_{REF_ADC}$, the exact value of V $_{REF_ADC}$ does not need to be known in the end application.

Follow these steps to compute a calibrated ADC reading:

1. Take the ADC reading at $V_{IN} = 90\% \times V_{REF}$ and $V_{IN} = 10\% \times V_{REF}$. The ADC readings for $10\%V_{REF}$ and $90\%V_{REF}$ are taken.

$$V_{REF}90 = 0.9(V_{REF_ADC})$$
 (5)

$$V_{REF}10 = 0.1(V_{REF_ADC})$$
 (6)

$$V_{\text{MEAS}}90 = ADC_{\text{MEASUREMENT}} \text{ at } V_{\text{REF}}90$$
 (7)

$$V_{\text{MEAS}}10 = ADC_{\text{MEASUREMENT}} \text{ at } V_{\text{REF}}10$$
 (8)

 Compute the ADC measured gain. The slope of the curve connecting the measured 10%V_{REF} and measured 90%V_{REF} point is computed and compared to the slope between the ideal 10%V_{REF} and ideal 90%V_{REF}. This result is the measured gain.

$$G_{MEAS} = \frac{V_{MEAS}90 - V_{MEAS}10}{V_{REF}90 - V_{REF}10}$$
(9)

3. Compute the ADC measured offset. The measured offset is computed by taking the difference between the measured $10\%V_{REF}$ and the (ideal $10\%V_{REF}$) × (measured gain).

$$O_{MEAS} = V_{MEAS} 10 - (V_{REF} 10 \times G_{MEAS})$$
 (10)

4. Compute the calibrated ADC readings.

$$V_{AD_MEAS} = Any V_{IN} ADC_{MEASUREMENT}$$
 (11)

$$V_{ADC_CAL} = \frac{V_{AD_MEAS} - O_{MEAS}}{G_{MEAS}}$$
 (12)

Any ADC reading can therefore be calibrated by removing the gain error and offset error. The measured offset is subtracted from the ADC reading and then divided by the measured gain to give a corrected reading. If this calibration is performed on a timed basis, relative to the specific application, gain and offset error over temperature are also removed from the ADC reading by calibration.

For example; given:

- 12-Bit ADC
- ADC Gain Error = +6LSB
- ADC Offset Error = +4LSB
- ADC Reference (V_{REF ADC}) = +5V
- Temperature = +25°C

Table 10 shows the resulting system accuracy.

Table 10. Bits of System Accuracy⁽¹⁾ (to 0.5LSB)

V _{IN}	ADC ACCURACY WITHOUT CALIBRATION	ADC ACCURACY WITH PGA112 CALIBRATION
10%V _{REF_ADC}	8.80 Bits	12.80 Bits
90%V _{REF_ADC}	7.77 Bits	11.06 Bits

(1) Difference in maximum input offset voltage for V_{IN} = 10%V_{REF_ADC} and V_{IN} = 90%V_{REF_ADC} is the reason for different accuracies.



APPLICATIONS: GENERAL-PURPOSE INPUT SCALING

Figure 70 example application that is an demonstrates the flexibility of the PGA for general-purpose input scaling. V_{IN0} is a ±100mV input that is ac-coupled into CH0. The PGA112/PGA113 is powered from a +5V supply voltage, V_S, and configured with the V_{REF} pin connected to $V_S/2$ (+2.5V). V_{CH0} is the ±100mV input, level-shifted and centered on V_S/2 (+2.5V). A gain of 20 is applied to CH0, and because of the PGA113 configuration, the output voltage at V_{OUT} is ±2V centered on V_S/2 (+2.5V).

CH1 is set to G = 1; through a resistive divider and scalar network, we can read $\pm 5V$ or 0V. This setting provides bipolar to single-ended input scaling.

Table 11 summarizes the scaling resistor values for R_A , R_X , and R_B for different ADC Ref voltages. V_{REF_ADC} is the reference voltage used for the ADC connected to the PGA112/PGA113 output. It is assumed the ADC input range is 0V to V_{REF_ADC} . The Bipolar Input to Single-Supply Scaling section gives the algorithm to compute resistor values for references not listed in Table 11. As a general guideline, R_B should be chosen such that the input on-channel current multiplied by R_B is less than or equal to the input offset voltage. This value ensures that the scaling network contributes no more error than the input offset voltage. Individual applications may require other design trade-offs.

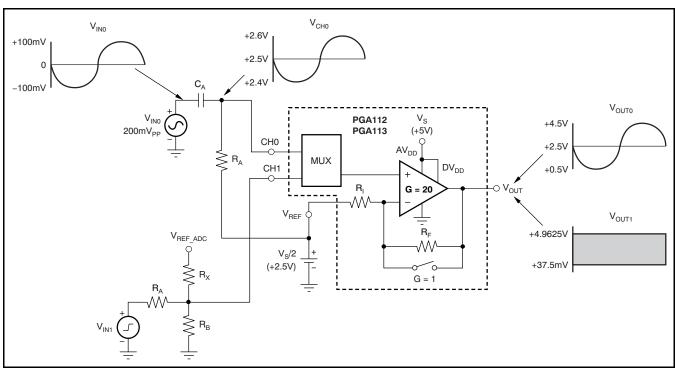


Figure 70. General-Purpose Input Scaling



Table 11. Bipolar to Single-Ended Input $Scaling^{(1)(2)}$

V _{REF_ADC} (V)	V _{IN1} (V)	CH1 INPUT	$R_A(k\Omega)$	$R_X(\Omega)$	$R_{B}(k\Omega)$
2.5	-5	0.047613	9.2	4.81k	10
	0	1.247613			
	5	2.447613			
2.5	-10	0.050317	3.16	2.4k	10
	0	1.250317			
	10	2.450317			
3	- 5	0.058003	13.5	5.76k	10
	0	1.498003			
	5	2.938003			
3	-10	0.059303	4.02	2.87k	10
	0	1.499303			
	10	2.939303			
4.096	- 5	0.082224	37	7.87k	10
	0	2.048304			
	5	4.014384			
4.096	-10	0.086018	6.49	3.92k	10
	0	2.052098			
	10	4.018178			
5	- 5	0.093506	24	965	10
	0	2.493506			
	5	4.893506			
5	-10	0.095227	9.2	4.81k	10
	0	2.495227			
	10	4.895227			

Scaling is based on 0.02(V_{REF_ADC}) to 0.98(V_{REF_ADC}), using standard 0.1% resistor values. Assumes symmetrical V_{IN} and symmetrical scaling for CH1 input minimum and maximum.



Bipolar Input to Single-Supply Scaling

Note that this process assumes a symmetrical V_{IN1} and that symmetrical scaling is used for CH1 input minimum and maximum values. The following steps give the algorithm to compute resistor values for references not listed in Table 11.

Step 1: Choose the following:

- a. $V_{REF\ ADC} = 2.5V$ (ADC reference voltage)
- b. $|V_{IN1}| = 5$

(magnitude of V_{IN}, assuming scaling is for ±V_{IN1})

c. Choose R_{B} as a standard resistor value. The input on-channel current multiplied by R_{B} should be less than the input offset voltage, such that R_{B} is not a major source of inaccuracy.

 $R_B = 10k\Omega$ (select as a starting value for resistors)

d. For the most negative V_{IN1} , choose the percentage (in decimal format) of $V_{\text{REF_ADC}}$ desired at the ADC input.

$$k_{VO-} = 0.02$$

(CH1 input =
$$k_{VO-} \times V_{REF\ ADC}$$
 when $V_{IN1} = -V_{IN1}$)

e. For the most positive V_{IN1} , choose the percentage (in decimal format) of V_{REF_ADC} desired at the ADC input. Since this scaling is based on symmetry, k_{VO+} must be the same percentage away from V_{REF_ADC} at the upper limit as at the lower limit where k_{VO-} is computed.

$$k_{VO+} = 1 - k_{VO-}$$

$$k_{VO+} = 1 - 0.02 = 0.98$$

(CH1 input =
$$k_{VO+} \times V_{RFF-ADC}$$
 when $V_{IN1} = +V_{IN1}$)

Step 2: Compute the following:

a. To simplify analysis, create one constant called k_{VO} .

$$k_{VO} = k_{VO+} - k_{VO-}$$

$$0.96 = 0.98 - 0.02$$

 A constant, g, is created to simplify resistor value computations.

$$g = \frac{k_{VO} \times V_{REF_ADC}}{2 \times |V_{IN1}| - k_{VO} \times V_{REF_ADC}}$$

$$0.315789474 = \frac{0.96 \times 2.5}{2 \times 5 - 0.96 \times 2.5}$$

c. R_A is now selected from the starting value of R_B and the g constant.

$$R_A = \frac{2 \times R_B \times g}{1 - g}$$

$$9.23077k\Omega = \frac{2 \times 10k\Omega \times 0.315789474}{1 - 0.315789474}$$

d. R_X can now be computed from the starting value of R_B and the computed value for R_A .

$$R_{X} = \frac{R_{B} \times R_{A}}{R_{B} + R_{A}}$$

$$4.81k\Omega = \frac{10k\Omega \times 9.23077k\Omega}{10k\Omega + 9.23077k\Omega}$$

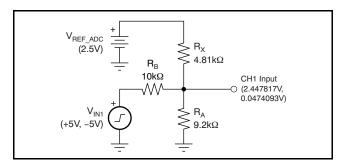


Figure 71. Bipolar to Single-Ended Input Algorithm

APPLICATIONS: HIGH GAIN/WIDE BANDWIDTH CONSIDERATIONS

As a result of the combination of wide bandwidth and high gain capability of the PGA112/PGA113 and PGA116/PGA117, there are several printed circuit board (PCB) design and system recommendations to consider for optimum application performance.

1. Power-supply bypass. Bypass power-supply pin separately. Use a ceramic capacitor connected directly from power-supply pin to the ground pin of the IC on the same PCB plane. Vias can then be used to connect to ground and voltage planes. This configuration keeps parasitic inductive paths out of the local bypass for the PGA. Good analog design practice dictates the use of a large value tantalum bypass capacitor on the PCB for each respective voltage.



2. Signal trace routing. Keep V_{OUT} and other low impedance traces away from MUX channel inputs that are high impedance. Poor signal routing can cause positive feedback, unwanted oscillations, excessive overshoot and ringing step-changing signals. If the input signals are particularly noisy, separate MUX input channels with guard traces on either side of the signal traces. Connect the guard traces to ground near the PGA and at the signal entry point into the PCB. On multilayer PCBs, ensure that there are no parallel traces near MUX input traces on adjacent layers; capacitive coupling from other layers can be a problem. Use ground planes to isolate MUX input signal traces from signal traces on other layers.

Additionally, group and route the digital signals into the PGA as far away as possible from the analog MUX input signals. Most digital signals are fast rise/fall time signals with low-impedance drive capability that can easily couple into the high-impedance inputs of the input MUX channels. This coupling can create unwanted noise that gains up to $V_{\rm OUT}$.

3. Input MUX channels and source impedance. Input MUX channels are high-impedance; when combined with high gain, the channels can pick up unwanted noise. Keep the input signal sources low-impedance (< 10kΩ). Also, consider bypassing input MUX channels with a ceramic bypass capacitor directly at the MUX input pin.</p>

Bypass capacitors greater than 100pF are recommended. Lower impedances and a bypass capacitor placed directly at the input MUX channels keep crosstalk between channels to a minimum as a result of parasitic capacitive coupling from adjacent PCB traces and pin-to-pin capacitance.

APPLICATIONS: DRIVING/INTERFACING TO ADCS

CDAC SAR ADCs contain an input sampling capacitor, C_{SH}, to sample the input signal during a sample period as shown in Figure 72. After the sample period, C_{SH} is removed from the input signal. Subsequent comparisons of the charge stored on C_{SH} are performed during the ADC conversion process. To achieve optimal op amp stability, input signal settling, and the demands for charge from the input signal conditioning circuitry, most ADC applications are optimized by the use of a resistor (R_{FII T}) and capacitor (CFILT) filter placed between the op amp output and ADC input. For the PGA112/PGA113, setting $C_{FILT} = 1nF$ and $R_{FILT} = 100\Omega$ yields optimum system performance for sampling converters operating at speeds up to 500kHz, depending upon application settling time and accuracy requirements.

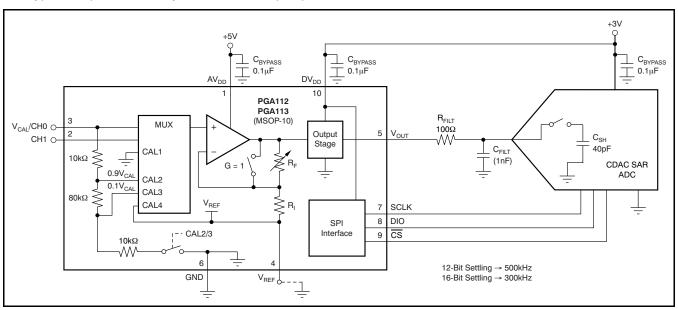


Figure 72. Driving/Interfacing to ADCs



POWER SUPPLIES

Figure 73 shows a typical mixed-supply voltage system where the analog supply, AVDD, is +5V and the digital supply voltage, DV_{DD} , is +3V. The analog output stage of the PGA and the SPI interface digital circuitry are both powered from DV_{DD}. When considering the power required for DVDD, use the Electrical Characteristics table and add any load current anticipated on V_{OUT}; this load current must be provided by DV_{DD}. This split-supply architecture ensures compatible logic with levels microcontroller. It also ensures that the PGA output cannot run the input for the onboard ADC into an overvoltage condition; this condition could cause device latch-up and system lock-up, and require power-supply sequencing. Each supply pin should be individually bypassed with a 0.1µF ceramic capacitor directly at the device to ground. If there is only one power supply in the system, AV_{DD} and DV_{DD} can both be connected to the same supply; however, it is recommended to use individual bypass capacitors directly at each respective supply pin to a single point ground. V_{OUT} is diode-clamped to AV_{DD} (as shown in Figure 73); therefore, set $\mathrm{DV}_{\mathrm{DD}}$ less than or equal to AV_{DD} + 0.3V. DV_{DD} and AV_{DD} must be within the operating voltage range of +2.2V to +5.5V.

At initial power-on, the state of the PGA is G=1 and Channel 0 active. **CAUTION:** For most applications, set $AV_{DD} \ge DV_{DD}$ to prevent V_{OUT} from driving current into AV_{DD} and raising the voltage level of AV_{DD} .

SHUTDOWN AND POWER-ON-RESET (POR)

The PGA112/PGA113 have a software shutdown mode, and the PGA116/PGA117 offer both a hardware and software shutdown mode. When the PGA is shut down, it goes into a low-power standby mode. The Electrical Characteristics table details the current draw in shutdown mode with and without the SPI interface being clocked. In shutdown mode, R_{F} and R_{I} remain connected between V_{OUT} and V_{REF} .

When $\mathrm{DV_{DD}}$ is less than 1.6V, the digital interface is disabled and the channel and gain selections are held to the respective POR states of Gain = 1 and Channel = $\mathrm{V_{CAL}}/\mathrm{CH0}$. When $\mathrm{DV_{DD}}$ is above 1.8V, the digital interface is enabled and the POR gain and channel states remain unchanged until a valid SPI communication is received.

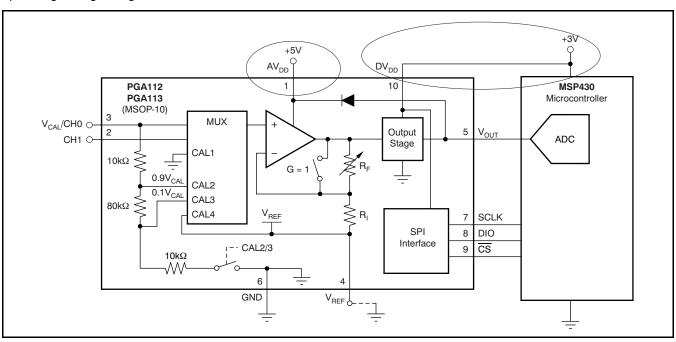


Figure 73. Split Power-Supply Architecture: AV_{DD} ≠ DV_{DD}





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PACKAGING INFORMATION

Orderable Device	Status ⁽¹⁾	Package Type	Package Drawing	Pins	Package Qty	e Eco Plan ⁽²⁾	Lead/Ball Finish	MSL Peak Temp (3)
PGA112AIDGSR	ACTIVE	MSOP	DGS	10	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR
PGA112AIDGSRG4	ACTIVE	MSOP	DGS	10	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR
PGA112AIDGST	ACTIVE	MSOP	DGS	10	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR
PGA112AIDGSTG4	ACTIVE	MSOP	DGS	10	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR
PGA113AIDGSR	ACTIVE	MSOP	DGS	10	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR
PGA113AIDGSRG4	ACTIVE	MSOP	DGS	10	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR
PGA113AIDGST	ACTIVE	MSOP	DGS	10	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR
PGA113AIDGSTG4	ACTIVE	MSOP	DGS	10	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR
PGA116AIPW	PREVIEW	TSSOP	PW	20	70	TBD	Call TI	Call TI
PGA116AIPWR	PREVIEW	TSSOP	PW	20	2000	TBD	Call TI	Call TI
PGA117AIPW	PREVIEW	TSSOP	PW	20	70	TBD	Call TI	Call TI
PGA117AIPWR	PREVIEW	TSSOP	PW	20	2000	TBD	Call TI	Call TI

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

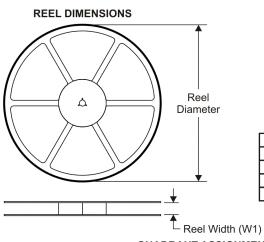
(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

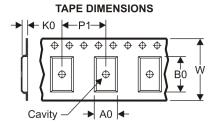
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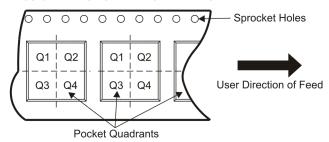
TAPE AND REEL INFORMATION





A0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

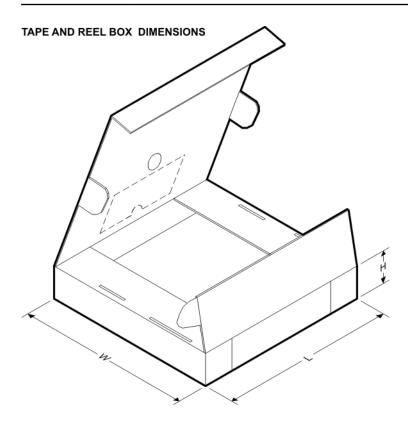
QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
PGA112AIDGSR	MSOP	DGS	10	2500	330.0	12.4	5.3	3.3	1.3	8.0	12.0	Q1
PGA112AIDGST	MSOP	DGS	10	250	180.0	12.4	5.3	3.3	1.3	8.0	12.0	Q1
PGA113AIDGSR	MSOP	DGS	10	2500	330.0	12.4	5.3	3.3	1.3	8.0	12.0	Q1
PGA113AIDGST	MSOP	DGS	10	250	180.0	12.4	5.3	3.3	1.3	8.0	12.0	Q1





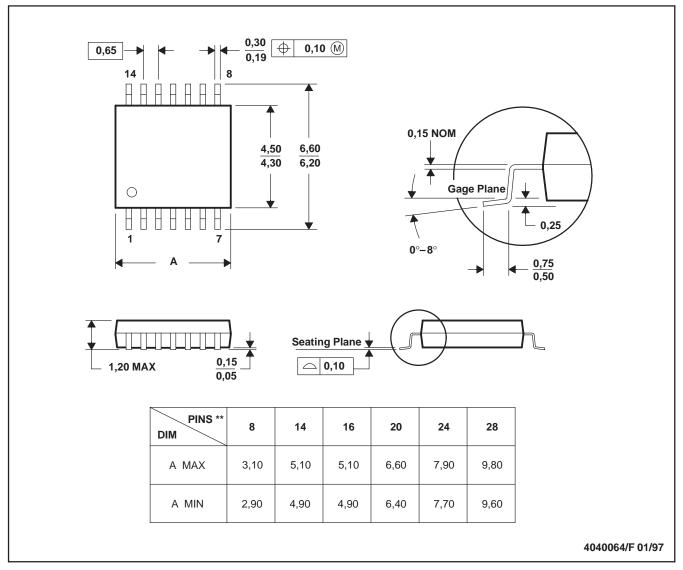
*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
PGA112AIDGSR	MSOP	DGS	10	2500	370.0	355.0	55.0
PGA112AIDGST	MSOP	DGS	10	250	370.0	355.0	55.0
PGA113AIDGSR	MSOP	DGS	10	2500	370.0	355.0	55.0
PGA113AIDGST	MSOP	DGS	10	250	195.0	200.0	45.0

PW (R-PDSO-G**)

14 PINS SHOWN

PLASTIC SMALL-OUTLINE PACKAGE



NOTES: A. All linear dimensions are in millimeters.

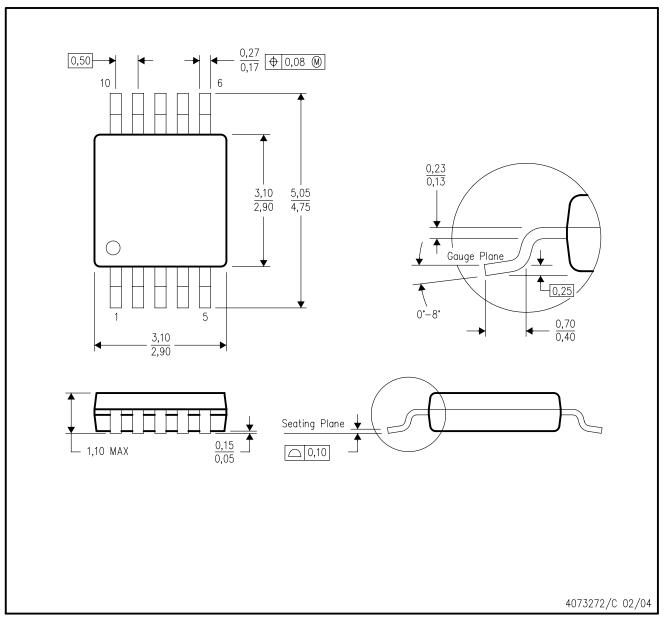
B. This drawing is subject to change without notice.

C. Body dimensions do not include mold flash or protrusion not to exceed 0,15.

D. Falls within JEDEC MO-153

DGS (S-PDSO-G10)

PLASTIC SMALL-OUTLINE PACKAGE



NOTES:

- A. All linear dimensions are in millimeters.
- B. This drawing is subject to change without notice.
- C. Body dimensions do not include mold flash or protrusion.
- D. Falls within JEDEC MO-187 variation BA.



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